Degradation of AB113 using combined photocatalysis and biological processes: Economic choice and enhanced removal of aromatic compounds



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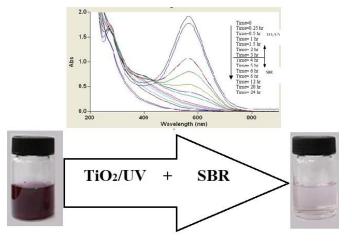
Dyes are important chemical compounds which are applied to textile, paper, food, printing, leather, cosmetics industries, and so on. Textile dyes are aromatic and hardly degradable compounds causing harmful effects such as toxicity, carcinogenesis, and mutagenesis. Conventional treatment processes such as biological processes, or adsorption to activated carbon are not very effective for textile wastewater treatment, and therefore advanced treatment process was extended. In this study, decolorization and mineralization of Acid Blue 113 were investigated using combined TiO₂/UV-SBR systems. Dye concentration in the effluent of photocatalytic reactor was selected via efficiency of dye removal, BOD₅/COD ratio, and energy consumption of alkali media. Three hours after applying the samples to the photocatalytic reactor, more than 80% of the dye was removed and the rest was decolorized approximately after passing bioreactor. Investigation of optimum condition leads to enhance the degradation of aromatic compounds. The results show that second order and Grau are the best models to describe the photocatalytic and biological kinetic data with higher correlation coefficients, respectively.



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Conflict of interest: The authors declare that they have no conflicts of interest.

GRAPHIC ABSTRACT



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Introduction

Approximately, 100,000 commercially available dyes and pigments are used in industries such as textile dyeing, cosmetics, and paper production, and around 700,000 tons of synthetic dyes are produced annually. Researchers report that about 10-15% of consuming dyes are lost in the effluent during dyeing processes^{1,2}. The wastewater emerging from textile industry has the lowest ratio of BOD₅: COD (<0.1)^{3,4}. Dyes change the color of water and prevent light diffusion, disturb photosynthesis and lead to destruction of aquatic ecosystem^{1,5}. Modern commercial dyes are very stable and contain a high composition ratio of aromatic rings⁶. Azo dyes are the most applied class of organics. The release of these compounds into the environment is undesirable; not only because of their color, but also because their breakdown products are toxic and/or mutagenic to life. Thus, wastewater containing synthetic azo dyes is considered a serious warning for the environment and removal of these pollutants has been attended in several researches⁶⁻⁸. However, conventional treatment techniques including physical, chemical, and biological, such as adsorption, filtration, coagulation, and chemical oxidation are unable to provide environmental standards of degradation^{1,9}. Advanced oxidation processes (AOPs) such as ozonation, electrochemical oxidation and photocatalytic methods are proper to mineralize dve wastewater¹⁰.

In the hybrid methods toxic and non-degradable chemicals endure chemical process, breakdown to compounds with less toxic nature and more biodegradable. For example, coupling both biological and chemical processes could be an efficient approach to decrease the cost of wastewater treatment, energy consumption, and complete degradation time^{11,12}. Recently, many coupled systems such as up-flow anaerobic sludge blanket (UASB) reactor¹³ and ozonation, Fenton's reagent with aerobic biological treatment, and ozonation^{14,15} with biological treatment¹¹ have been studied to treat different kinds of industrial wastewaters such as effluents from textile industry, dye house liquors, olive mill, and polyester resin production.

In recent years, application of advanced oxidation methods (AOPs) such as photocatalytic reactions have been expanded for removing non-biodegradable and toxic pollutants ^{16,17}. When photo-catalyst such as titanium dioxide (TiO₂) absorbs ultraviolet radiation from sunlight or illuminated light source, it will produce pairs of electrons and holes. The electron of the valence band becomes excited when illuminated by light. Also, the excess energy of this excited electron promoted the electron to the conduction band. The generated holes oxidize the organic compounds and produce positive charged molecules (R⁺), which would react with OH⁻ and finally the hydroxide radical is generated ¹⁸. Also, photocatalytic process gradually breaks down the contaminant molecules under room temperature and pressure, no residue of the original material remains and therefore no sludge requiring disposal to landfill is produced ¹⁹.

In the past two decades, significant studies have been done using microorganisms to remove environmental contaminants from textile wastewater. Different microorganisms such as aerobic and anaerobic bacteria and fungi could degrade azo dyes^{20,21}. Sequencing batch reactor (SBR) is a wastewater treatment process based on the activated sludge system. The operating cycle is divided into five phases, including filling, aeration-reaction, settling, decanting and idle. With respect to the application, SBR has been successfully employed in biodegradation of both municipal and industrial wastewater^{22,23}.

Wang and his colleagues worked on Reactive Black (RB5) solution degradation using coupled electrochemical/photocatalyst degradation processes. Rapid decolorization rate of RB5 solution (55 and 110 μ mol/dm³) was yielded by applying the electrochemical oxidation method at pH 4 and current density of 277 A/m² with enough electrolytes (2 g NaCl/dm³). In addition, more than 95% of dye was removed for 4 minutes. In photocatalytic method, 63% and 23% of RB5 was degraded by immobilized TiO₂ within 5 hours for initial dye concentration of 55 and 110 μ mol/ dm³, respectively. By combining the two methods, the researchers concluded that the concentration of the dye and TOC was effectively reduced²⁴. In another study, Chengyuan

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and his coworkers²⁵ studied effect of cephalexin after heterogeneous Fenton-like pretreatment on the performance of anaerobic granular sludge and activated sludge. They concluded that Fe₃O₄ NPs Fenton-biotreatment was an effective approach in treating cephalexin. Also, Humic acid in LB-EPS and TB-EPS decreased after pretreatment and Rhodobacteraceae have the most significant increase at pretreatment condition²⁵.

Acid dyes which are organic sulfonic acids with high solubility are the most widely used chemicals in the industry for dying different fibers such as cotton, rayon, and polyester⁶. Currently, these types of dyes are increasingly used in I.R. Iran. According to the statistics reports, 141000 tons of acid dyes were imported in 2011²⁶.

The main objective of the present study was to investigate the performance of immobilized photocatalytic reactor on concrete surface as a pre-treatment unit to enhance dye removal by breakdown of aromatic rings. For this reason, the combined photocatalytic—biological process was studied for dye degradation, which not only makes it possible but also was more economical considering the high costs of using merely chemical processes. The effects of variables, including initial pH, dye concentration, energy consumption, irradiation intensity and BOD₅/COD ratio were studied by changing each in turn while keeping the other parameters constant.

Method

Material properties

Acid Blue 113 (AB113) (molecular weight=681.6 g/mol, solution pH=6-9, chemical structure: diazo) was purchased from Alvan Sabet Company (Tehran, Iran) and used without any purification (Figure 1). The photocatalyst was P25 titania from Degussa Company (density=5 g/cm³, particle size=21 nm, ratio of anatase to rutile=80:20). All the materials for biological system feeding were in analytical grade (Merck, Germany). Also, K₂CrO₇, AgSO₄, HgSO₄, and NaOH (Merck, Germany), were used for the COD measurement. UV-C lamps were purchased from Philips Company.

The applied spectrophotometer was Carry 50, Varian Co. The COD reactor and BOD meter which have been used for determining the amounts of organic pollution were DRB200, Hatch Co. and OxiTop, WTW Co., respectively. Also, ultrasound was used for dispersing nano particles (Fungilab, UE-6SFD) and H₂SO₄ and NaOH were employed for pH adjustment in the range of 3-11. In addition, pH meter (Metrohm, 691) and centrifuge (CE145, Shimi Fan Co.) have been applied.

Fig 1. Structure of acid blue 113

Configuration of combined system

The combined lab-scale photocatalytic—SBR system used for the mineralization of biorecalcitrant AB113 has been designed and constructed in the environmental engineering laboratory (Figure 2). The photocatalytic reactor was a plastic container (length=0.23 m, width=0.16 m, height=0.05 m), inside which a concrete bed with 0.008 m thickness was located.

An immobilized ($TiO_2=40 \text{ g/m}^2$) system was applied by concrete glue²⁷. To reach the maximum percentage of UV irradiation reflection and safety aspects, inner and outer surfaces of the reactor were covered with aluminum foil. To investigate the effect of UV-C irradiation intensity, the UV-C lamps with power of 30, 90, 150 and 210 Watts were used (for instance, symbol $P_{UVC}=30$ W means UV-C lamp with 30 Watts power). Total volume of dye solution was 25 cm³ in each reactor. The bioreactor consists of a sequencing batch reactor made of Plexiglas with inner diameter of 0.1 m, height of 0.7 m, and 3 L effective volumes.

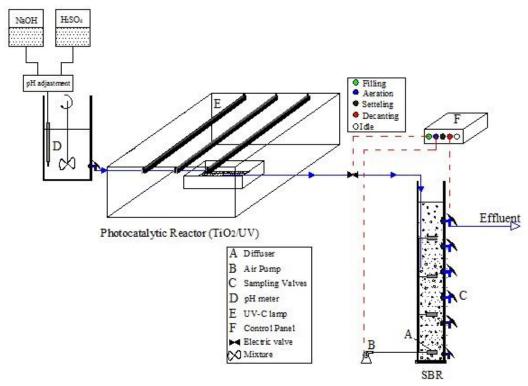


Fig 2. Schematic of the experimental photocatalytic-biological reactors used in this study

Composition of synthetic wastewater

The synthetic wastewater for photocatalytic reactor was prepared with different concentration of AB113 including 50, 75, 100, 150 and 200 mg/L in tap water. C and C_0 were used as a dye concentration and initial dye concentration, respectively.

A mineral nutrients solution was added separately to the bioreactor that included nitrogen and phosphorus source (MgSO₄.7H₂O, FeCl₃.6H₂O and Na₂MoO₄.2H₂O) to keep the C/N/P ratio at 100:5:1. The sludge was prepared from sanitary wastewater (Shahrak Gharb wastewater treatment plant, Tehran, Iran). The adaptation period lasted 120 days (the initial COD=200 mg O₂/L). During this time, a combination of dye and glucose was used as feed. Also, a 10% increase of dye followed by the same decrease in glucose amount was done in each step of system feeding. In the main experiments, only dye was used as feed for the reactors. After the adaptation step, dye concentration was gradually increased to 200, 250, 300, 400 and 500 mg/L. The loading repetition was continued during each increase in dye concentration until reaching a stable state. The changes in COD removal were trivial because of the adaptation of microorganisms with the dye.

Also, during the operation period, mixed liquor suspended solids (MLSS) and sludge volume index (SVI) reached a nearly constant amount of 1837 ± 339 mg/L and 68 ± 12 cm³/g of MLSS, respectively (Figure 3).

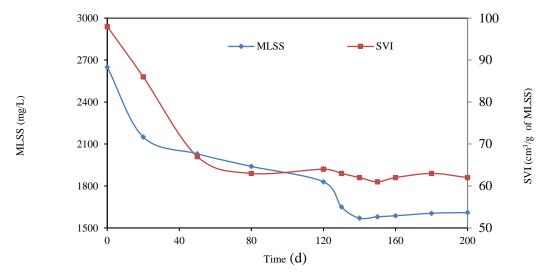


Fig 3. Changes in MLSS and SVI in SBR system

At the beginning of the adaptation period, because of the difficulty of dye degradation, the amount of MLSS and SVI decreased with time, and then tended to gradually increase. The variations in both MLSS and SVI were the same. The characteristics of the SBR system for different concentrations of dye are shown in Table1.

Table 1. Time ranges of SBR system for different (COD total=200 mg O₂/dm₃)

Time (min)	COD dye/COD total		
Stage	Less than 0.75	0.25 - 0.75	More than 0.25
Filling	2	2	2
Aeration-reaction	180	420	1380
Settling	20	20	20
Decanting	8	8	8
Idle	30	30	30

Analytical methods and procedures

Dye concentration was determined by measuring the absorbance of the test samples at the maximum absorbance wavelength of AB113 (λ_{max} :566 nm) using UV–Vis spectrophotometer. Before the analysis, samples withdrawn from the treatment systems were centrifuged at 3000 rpm for 10 min. According to the standard methods²⁷, COD and BOD₅ analysis was carried out with COD and BOD reactor. BOD was measured by standard method 5210 B (5-day BOD test) according to Sawyer and McCarty²⁷. The BOD measurement with OxiTop® is based on pressure measurement in a closed system: The micro-organisms in the sample consume the oxygen and generate CO₂ in the process. This is absorbed with NaOH. This will cause a vacuum pressure, which can be determined as a measured value in mg/L BOD. All experiments were conducted up to three times at room temperature (22 ± 1°C).

Results and Discussion

Effect of initial pH on TiO₂/UV process

The initial pH is one of the effective parameters influencing TiO_2/UV process that is shown in Figure 4. According to the results, 33.4, 51.9, 81.8 and 84.1% of AB113 was removed in 5 hours at pH 3, 6.5 (neutral), 9 and 11, correspondingly. The optimum pH was observed in the alkali condition due to more and reliable generation of hydroxide radicals^{19,28}.

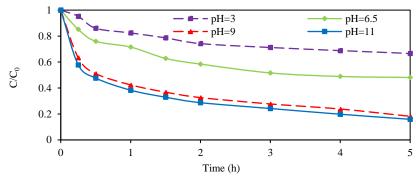


Fig 4. Effect of initial pH on the decolorization of AB113 solution by TiO_2/UV ($TiO_2=40$ g/m², $C_0=50$ mg/L, $P_{UVC}=30$ W)

In pH = 3, adsorption of dye molecules onto TiO_2 surface has an important role in dye removal because of the difference in surface charge between TiO_2 particles and dye molecules (PZC of TiO_2 is at pH 6.8)²⁹. At the first hours, suitable removal efficiency was observed at pH=3, which can be explained by more effect of OH^0 as compared to hole oxidizing. Also, changes of pH were monitored during the process to justify possibly generated intermediates³⁰. In this research, the pH of different media (alkali, neutral, and acidic) was trended to neutral during the process time (Figure 5). The optimum pH was found to be around 9 by considering dye removal efficiency, the energy costs, NaOH consumption and effluent pH.

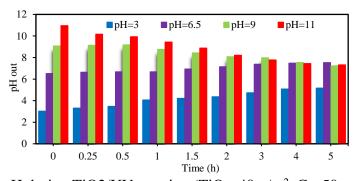


Fig 5. Changes of pH during TiO2/UV reaction (TiO₂=40 g/m², C₀=50 mg/L, P_{UVC}=30 W)

Effect of UV-C intensity on TiO₂/UV process

According to the results, dye removal increased in high irradiation intensity (Figure 6). Numbers of emitted photons were enhanced by increasing intensity of UV irradiation. But, when UV-C irradiation intensity was more than special value, the removal efficiency remained constant. The reason was that this intensity was equal to maximum energy for exciting immobilized TiO₂ on a concrete bed. Thus, 90 Watts was selected as the optimum UV-C irradiation intensity.

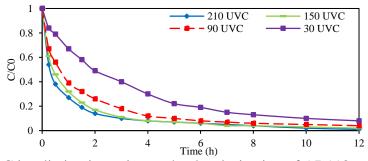


Fig 6. Effect of UV-C irradiation intensity on the decolorization of AB113 solution by TiO_2/UV ($TiO_2=40 \text{ g/m}^2, \text{ pH=9}, C_0=50 \text{ mg/L}$)

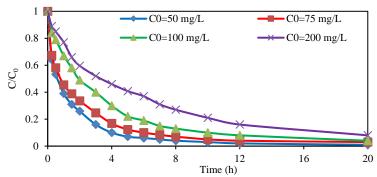


Fig 7. Effect of initial dye concentration on the removal of AB113 by TiO_2/UV ($TiO_2=40$ g/m², pH=9, $P_{UVC}=90$ W)

Effect of initial dye concentration on TiO2/UV process

According to Figure 7, 83.4, 77.9, 59.2 and 42.8% of AB113 was removed in 5 hours when dye concentration amounted to 50, 75, 100 and 200 mg/L, respectively. At high concentrations, more dye was adsorbed onto the TiO₂ surface. Consequently, the UV irradiation into the dye particle was hindered. In addition, by increasing the concentration of the dye, active sites onto the nano particles surface would be more occupied. Also, a significant amount of UV was absorbed by the dye molecules rather than TiO₂ particles¹⁹.

According to what was mentioned above, the concentration of OH* was decreased by increasing the concentration of the dye. Therefore, the efficiency of the catalytic reaction was reduced¹⁹. The presumed reason was that some photocatalytic reactions occurred, which caused degradation and removal of intermediates^{31,32}. Whereas dye removal in a short time could not be a logical selection for optimum concentration and effluent of photocatalytic reactor discharge to a biological system, then COD/COD₀, BOD₅/COD and energy consumption were investigated. As is evident from (Figure 8), the COD/COD₀ decreased at the first 20 min which can be contributed to the breaking down of N=N bond, and then it was enhanced due to degradation and simplification of the available compounds. In the following, oxidants are expected to substantially improve the degradation rates of products and as a result the rate of COD/COD₀ decreased during the treatment process. In addition, BOD₅/COD was measured at inflection and pick points (Figure 9). According to Equation (1)³³, the amount of energy consumption could be calculated to choose the suitable concentration based on influent BOD/COD in SBR.

$$EC/C=(W.t)/(C_{in}-C_{out})$$
(1)

Whereas W is energy consumption kW, t shows the time of radiation in hour, EC/C is the used energy for removal of pollutant in kWh.L/mg. C in and C out are the initial and final concentration in mg/L after photocatalytic process, respectively.

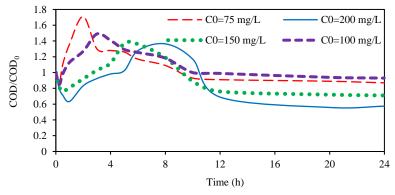


Fig 8. COD removal for different initial concentration of AB113 by TiO₂/UV (TiO₂=40 g/m², pH=9, P_{UVC}=90W)

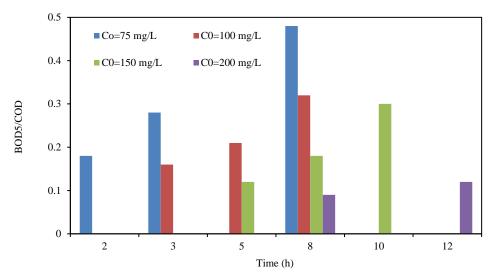


Fig 9. BOD₅/COD ratio for different initial concentration of AB113 in TiO₂/UV process (TiO₂=40 g/m², pH=9, P_{UVC}=90 W)

According to Figure 10, the amounts of 4.42, 9.35 and 7.8 Wh. L/mg were obtained for 75, 100 and 150 mg/L initial dye concentrations for the same BOD_5/COD (around 0.4), respectively. Thus, after 3 hours 75 mg/L dye was added to the bioreactor.

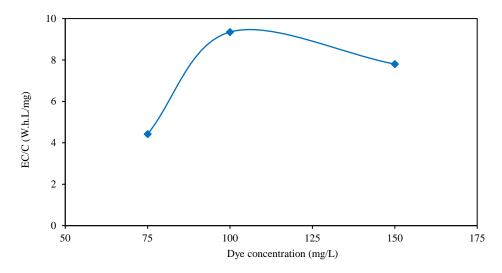


Fig 10. Energy consumption for different initial concentration of AB113 in TiO_2/UV process $(TiO_2=40 \text{ g/m}^2, \text{pH}=9, P_{UVC}=90 \text{ W})$

Capability investigation of combined system

Figure 11, Tables 2 and 3 show the absorption spectra for synthetic wastewater in the combined system and both photocatalytic and biological systems influent and effluent characteristics, respectively. There was 80% decolorization in the photocatalytic reactor after 3 hours. The residual color was completely removed, and the COD value was significantly diminished in the biological reactor. Also, the COD, BOD₅ and BOD₅/COD values increased in the effluent. This means that the dye complex molecules have been degraded and can be treated by the biological system. According to the results, the effluent from SBR has the environmental standard discharge concentration after about 20 hours.

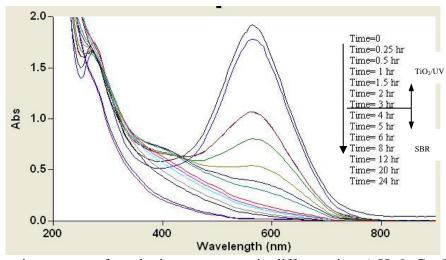


Fig 11. Absorption spectra of synthetics wastewater in different time (pH=9, C₀=50 mg/L)

Table 2. Influent and effluent parameters of photocatalytic reactor after 3 hours

Parameter	Influent	Effluent
Dye concentration (mg/L)	75	13.4
COD (mg O ₂ /L)	136.2	176.8
$BOD_5 (mg O_2/L)$	10	50
BOD ₅ /COD	0.08	0.4

Table 3. Influent and effluent parameters of bioreactor after 20 hours

Parameter	Influent	Effluent
Dye concentration (mg/ L)	13.4	0.3
COD (mg/L)	176.8	52.3
BOD ₅ (mg/L)	50	25
MLSS (mg/L)	1837±339	
MLVSS ¹ (mg/L)	1507±273	
MLVSS/MLSS	82.1±1.3	
SVI (cm³/g of MLSS)	68 ± 12	

Investigation of AB113 degradation

Decolorization is not the actual degradation of dye, since breaking specific bonds in molecule causes decolorization. Thus, after optimizing the parameters, in order to have more accurate consideration, UV-Vis absorption was determined at wavelengths 566, 255, 276³⁴, and 271 nm which were related to the known compounds AB113, benzene, naphthalene, and phenol, respectively^{28,35}. As shown in Figure 12, after 3 hours (effluent of photocatalytic reactor), removal of AB113, benzene, naphthalene, and phenol were 82.1, 11.3, 5.4, and 6.6% percent, respectively. Also, after 20 hours (effluent of bioreactor), those ratios reached 99.3, 27.2, 19.7 and 22.4 %, respectively. The presumed reason for increasing the removal of aromatic compounds is their degradation by adapted microorganisms or adsorption onto sludge due to hydrophobic structure.

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¹ Mixed Liquor Volatile Suspended Solids

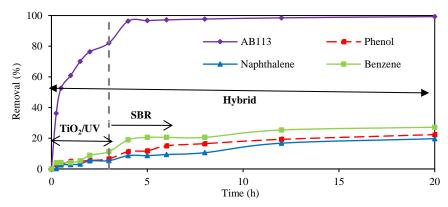


Fig 12. Comparison of removal between dye, phenol, naphthalene, and benzene (pH=9, C_0 =50 mg/L)

Kinetic study

Reactions in a photocatalytic reactor were categorized as zero-order, Langmuir-Hinshelwood (first-order) and the second-order reactions³⁶. Considering the optimum pH at 9, PZC of TiO_2 (at pH=6.8) and anionic structure of the dye molecule, it was observed that in this case absorbance was not the efficient factor. According to the results (Figure 13), the second-order kinetic of reaction had a decent agreement with the experimental data (R^2 =0.989).

Three kinetic models such as first-order, Grau and Stover–Kincannon have been also applied for the biological reactors 37,38 . According to the results, the decolorization kinetic was found to follow Grau model with a higher correlation coefficient of 99.8 %. In Grau model, θ_H , E are hydraulic retention times (h) and removal rate, respectively.

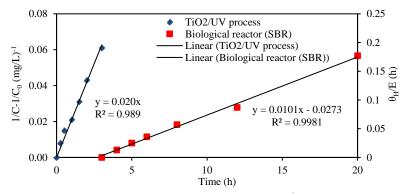


Fig 13. Graphic representation of kinetic models (TiO₂=40 g/m², C₀=75 mg/L, pH=9, P_{UVC}=90 W, MLSS=1600 mg/L, DO²=2.8 mg/L)

Conclusion

Since the biological systems have limitations for dye removal, using combined systems is essential. The feasibility of using a combined method involving photocatalyst, followed by the biological treatment for dye removal was confirmed. According to the results, dye concentration in the effluent of photocatalytic reactor (75 mg/L) was selected via BOD₅/COD (0.4) ratio and energy consumption in alkali media. Furthermore, more than 80 % of the dye was removed after 3 hours and the residual color was removed after passing through bioreactor. Also, second order and Grau models were selected as the kinetic model for photocatalytic and biological reactors, correspondingly.

² Dissolved Oxygen

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Author contributions

All authors contributed to the study's conception and design. Material preparation, data collection and analysis were performed by [Roya Nayebi Gavgani], [Bita Ayati] and [Hossein Ganjidoust]. The first draft of the manuscript was written by [Bita Ayati] and all authors commented on previous versions of the manuscript. All authors read and approved the final manuscript.